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# Fabrication of oxidation-resistant $\beta\mbox{-FeSi}_2$ film on $Mg_2Si$ by RF magnetron-sputtering deposition

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#### ABSTRACT

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1. Introduction

The intermetallic compound Mg<sub>2</sub>Si has been considered as a potential environment-friendly high-performance thermoelectric material [1–12], because it is non-toxic, lightweight, and it has high electron mobility; in addition, the raw materials used to manufacture it are inexpensive. Thermoelectric materials should have a large Seebeck coefficient *S*, small electrical resistivity  $\rho$ , and small thermal conductivity  $\kappa$ . Impurity doping drastically affects the thermoelectric properties of Mg<sub>2</sub>Si and its solid solution, and therefore, it is essential to determine suitable dopants for Mg<sub>2</sub>Si. In many experimental studies, Mg<sub>2</sub>Si has been doped with impurities with the objective of improving its thermoelectric figure of merit *Z*.

Oxidation is one of the primary mechanisms for the degradation of high-temperature Mg<sub>2</sub>Si thermoelectric devices. However, few studies have attempted to clarify this mechanism. Therefore, it is essential to understand the oxidation mechanism of Mg<sub>2</sub>Si in order to develop new oxidation-resistant films.  $\beta$ -FeSi<sub>2</sub> has an orthorhombic structure (space group: *Cmca*), and it is also an environment-friendly silicide semiconductor [13]. Moreover,  $\beta$ -FeSi<sub>2</sub> exhibits excellent oxidation-resistance in the high-temperature region below 800 °C [14,15]. Therefore,  $\beta$ -FeSi<sub>2</sub> can be considered as a potential candidate for use as an oxidationresistant coating material for Mg<sub>2</sub>Si. The formation of  $\beta$ -FeSi<sub>2</sub> films

has been attempted using various methods, and it has been success-

We study the oxidation of  $Mg_2Si$  and analyze its kinetics using the Johnson–Mehl–Avrami (JMA) equation.

Above 450 °C, Mg<sub>2</sub>Si reacts with O<sub>2</sub> in air to yield MgO and Si. The Avrami exponent (*n*) is equal to  $\sim$ 0.5,

and it depends on the reaction temperature and time; this indicates that the oxidation is controlled by

the diffusion-controlled reaction. In order to improve the oxidation-resistance of Mg<sub>2</sub>Si,  $\beta$ -FeSi<sub>2</sub> films

were fabricated on sintered Mg<sub>2</sub>Si samples by RF magnetron-sputtering deposition at RT followed by post-annealing at 600 °C in vacuum. An oxide layer having a thickness of  $8 \pm 3 \,\mu$ m was observed on the

uncoated Mg<sub>2</sub>Si samples after heat treatment in air at 600 °C for 3 h. However, no oxide layer was formed

on Mg<sub>2</sub>Si samples coated with 0.7- $\mu$ m thick  $\beta$ -FeSi<sub>2</sub> films. The  $\beta$ -FeSi<sub>2</sub> layer effectively prevented the

has been attempted using various methods, and it has been successfully formed on a glass plate, Si single crystal, and polycrystalline alumina by the RF magnetron-sputtering method [16–22].

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In the present study, we investigate the oxidation of Mg<sub>2</sub>Si and analyze its kinetics using the Johnson–Mehl–Avrami (JMA) equation. In order to improve the oxidation-resistance of Mg<sub>2</sub>Si,  $\beta$ -FeSi<sub>2</sub> films were fabricated on sintered Mg<sub>2</sub>Si samples by RF magnetron-sputtering deposition and then the oxidation-resistance of the samples was evaluated.

#### 2. Experimental

diffusion of oxygen at 600 °C and improved the oxidation-resistance of Mg<sub>2</sub>Si.

0.5 g of Mg<sub>2</sub>Si powder (purity: >99.5%; size: <20 mesh; Mitsuwa Chemical Co., Osaka, Japan) was pressed into pellets (diameter: 13 mm) at 60 MPa using a hand press and then fired in air to 200-800 °C with dwell times of 6 min to 4 h in an open crucible. The heating rate was 20 °C/min. Sintered dense Mg<sub>2</sub>Si samples were fabricated using the spark plasma sintering (SPS) method [7-13]. The constituent Mg (purity: >99.9%; size: <180  $\mu m$ ; Kojundo Chemical Laboratory Co. Ltd.; Saitama, Japan) and Si (purity: >99.999%; size: <75 µm, Kojundo Chemical Laboratory Co., Ltd.; Saitama, Japan) powders were ground together and then heated at 1053 K for 10 min at 20 MPa in a graphite die (diameter: 30 mm) in vacuum (<4 Pa) by the SPS method at a heating rate of  $\sim$ 50 K/min. The density of the annealed samples was more than 99% of the theoretical value. The surfaces of the sintered Mg<sub>2</sub>Si samples were polished with a 1200 grid SiC paper prior to sputtering. Fe-Si films were deposited by RF magnetron-sputtering (sputtering power: 400 W; model HSR-551S, Shimadzu Corporation, Kyoto, Japan) on the Mg<sub>2</sub>Si sample (temperature: RT) under an Ar atmosphere (pressure: 0.133 Pa). The sputtering target was a polycrystalline β-FeSi<sub>2</sub> disk (diameter: 100 mm).

The Fe–Si films and the oxidation of the sintered Mg<sub>2</sub>Si samples were characterized by using a scanning electron microscope (model JSM-6460LA, JEOL, Tokyo, Japan) at 20 kV with a working distance 20 mm. A phase analysis was carried out by X-ray powder diffraction (XRD; model RINT 2500, Rigaku, Tokyo) using CuK<sub>\alpha</sub> radi-

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Fig. 1. XRD patterns of products obtained by firing of  $Mg_2Si$  pellet in air at 800  $^\circ\text{C}$  for 12 h.



Fig. 2. TG/DTA curves of Mg<sub>2</sub>Si in air at a heating rate of 10 °C/min.

ation at 40 kV and 50 mA. Phase identification was accomplished by comparing the experimental XRD patterns with the standards compiled by the International Center for Diffraction Data (ICDD). In order to study the oxidation mechanism of Mg<sub>2</sub>Si in detail, thermogravimetric analysis and differential thermal analysis (TGA/DTA; model TGA/DTA 320, Seiko Instruments Inc., Chiba, Japan) of the Mg<sub>2</sub>Si powder was carried out at a heating rate of 10 °C/min in air flowing at 300 ml/min. The thermal expansion of sintered dense Mg<sub>2</sub>Si, fabricated by the SPS method, was measured on a bar (4 mm × 4 mm × 13 mm) using a thermal mechanical analyzer (model TMA 8310, Rigaku, Tokyo, Japan) in N<sub>2</sub> flowing at 100 ml/min at a heating rate of 5 °C/min in the temperature range of 25-300 °C.

#### 3. Results and discussion

#### 3.1. Oxidation behavior of Mg<sub>2</sub>Si

Fig. 1 shows XRD patterns of the products obtained by the firing of a Mg<sub>2</sub>Si pellet in air at 800 °C for 12 h. The XRD analyses revealed the presence of MgO (ICDD Card #45-0946), Si (ICDD Card #27-1402), and unreacted Mg<sub>2</sub>Si (ICDD Card #35-0773). The following reaction occurred between Mg<sub>2</sub>Si and O<sub>2</sub> at 450 °C:

$$Mg_2Si(s) + O_2(g) \rightarrow 2MgO(s) + Si(s)$$
(1)

At the beginning of the reaction, the outer portions of the pellets were brown, suggesting that a Si phase had formed, and the inside of the pellet was blue-black, which is characteristic of  $Mg_2Si$ .

Fig. 2 shows TGA/DTA curves of Mg<sub>2</sub>Si obtained under air flowing at a rate of 300 ml/min and at a heating rate of 10 °C/min. The weight of Mg<sub>2</sub>Si remained constant below ~450 °C. The majority of the weight gain of Mg<sub>2</sub>Si occurred above ~500 °C due to the oxidation reaction. Our DTA result is in good agreement with previous experimental results [23,24].

The reaction kinetics of the oxidation mechanism was examined. Hancock and Sharp [25] proposed the application of the



Fig. 3. Fraction reacted, y, as a function of reaction time at various temperatures during oxidation of  $Mg_2Si$ .

generalized Avrami formula [26–28] to the study of solid-state kinetics data. In general, the Johnson–Mehl–Avrami (JMA) kinetics equation is given by:

$$y = 1 - \exp[-(kt)^n], \tag{2}$$

where y is the fraction reacted at a given temperature in time t; k, the reaction rate constant; and n, the Avrami exponent.

$$k = A \exp\left(-\frac{E_a}{RT}\right);\tag{3}$$

here, k is related to the activation energy of the process,  $E_a$ , through the Arrhenius temperature dependence.

The logarithmic equation that results from the rearrangement of Eq. (2) is

$$\ln\left[\ln\left(\frac{1}{1-y}\right)\right] = n\ln k + n\ln t,\tag{4}$$

where y was determined using Eq. (5) by measuring the weight of the pellet before and after firing in air.

$$Mg_2Si(s) + yO_2(g) \rightarrow (1 - y)Mg_2Si(s) + 2yMgO(s) + ySi(s)$$
(5)

Fig. 3 shows the reacted fraction as a function of the reaction time of  $Mg_2Si$  oxidation. The reacted fraction increases with



Fig. 4. Reaction kinetics fitted by the Johnson–Mehl–Avrami equation for the oxidation of  $Mg_2Si$ .

increasing with reaction time and temperature. The reacted fractions at 500, 550, 600, and 650 °C at a dwell time of 2 h are 8.6, 36.7, 49.8, and 68.8%, respectively. Fig. 4 shows that the plot of the  $\ln[\ln(1/(1-y))]$  vs.  $\ln(time)$  for Mg<sub>2</sub>Si oxidation is a straight line at the fraction reacted above ~20%. The values of *n* for reaction temperatures of 500, 550, 600, and 650 °C are 0.36, 0.71, 0.48, and 0.36, respectively. From the slope of the  $\ln k-1/T$  plot, the activation energy  $E_a$  is determined to be 177 kJ/mol. A value close to 0.5 indicates that the rate-controlling step is a diffusion mechanism [25,29]. Therefore, it is important to block the diffusion of oxygen onto the surface of Mg<sub>2</sub>Si in order to prevent the oxidation of Mg<sub>2</sub>Si.

## 3.2. $\beta$ -FeSi<sub>2</sub> film deposited on sintered Mg<sub>2</sub>Si samples by RF magnetron-sputtering method

In order to improve the oxidation-resistance of Mg<sub>2</sub>Si, β-FeSi2 films were fabricated on sintered Mg2Si samples by RF magnetron-sputtering deposition at room temperature (RT) followed by post-annealing at 600 °C for 1 h in vacuum. Fig. 5 shows XRD patterns of Fe-Si film deposited on sintered Mg<sub>2</sub>Si samples before and after annealing at 600 °C for 1 h in vacuum (<0.1 Pa). No XRD diffraction peaks except those of the Mg<sub>2</sub>Si phase are observed in the as-sputtered samples, indicating that Fe–Si films deposited at RT have an amorphous structure. After annealing at 600 °C, the diffraction peaks of the  $\beta$ -FeSi<sub>2</sub> phase as well as Mg<sub>2</sub>Si phase are detected in the XRD pattern. The coefficient of thermal expansion (CTE) of SPS-sintered polycrystalline Mg<sub>2</sub>Si in the temperature range of 25–300 °C is  $16.5 \times 10^{-6}$  °C<sup>-1</sup>; this value is much higher than that of  $\beta$ -FeSi<sub>2</sub>  $(7.7 + 5.5 \times 10^{-3} T) \times 10^{-6} \circ C^{-1}$  (*T* = absolute temperature) [30]. Scanning electron microscopy analysis of the surface of β-FeSi<sub>2</sub> films deposited on sintered Mg<sub>2</sub>Si samples indicates that peeling or partial removal of film occurs when the films are thicker than  $1\,\mu m$  because of the difference between the CTE values of  $\beta$ -FeSi<sub>2</sub> and Mg<sub>2</sub>Si. No peeling or partial removal of film was observed when the film thickness was  $0.7 \,\mu$ m.



Fig. 5. XRD patterns of Fe–Si films deposited on sintered Mg<sub>2</sub>Si samples with and without annealing at 600  $^{\circ}$ C in vacuum: (a) as-deposited; and (b) with annealing at 600  $^{\circ}$ C for 1 h.

Fig. 6 shows scanning electron micrographs of the cross-sections of sintered Mg<sub>2</sub>Si samples with and without  $\beta$ -FeSi<sub>2</sub> films after heat treatment in air at 600 °C for 1–3 h. The thickness of the oxide layer that was formed on the uncoated Mg<sub>2</sub>Si samples was 5 ± 2  $\mu$ m and 8 ± 3  $\mu$ m after 1 and 3 h, respectively. The surface of sintered Mg<sub>2</sub>Si samples was brown, suggesting the formation of Si phase. The oxide layer was composed of Si and MgO, and it had a very small grain size of <~200 nm. Because the oxide layer was porous, the oxidation reaction proceeded through the diffusion of oxygen at the interface between Mg<sub>2</sub>Si and the oxide layer.

However, in case of the Mg<sub>2</sub>Si samples coated with 0.7  $\mu$ m thick  $\beta$ -FeSi<sub>2</sub> films, no oxide layer was formed after heat treatment at 600 °C in air for 1–3 h. Scanning electron microscopy analysis of the surface of the  $\beta$ -FeSi<sub>2</sub> films coated on sintered Mg<sub>2</sub>Si samples indicated the absence of pinholes and cracks. Therefore, we can conclude that the  $\beta$ -FeSi<sub>2</sub> layer effectively prevented the diffusion



**Fig. 6.** Scanning electron micrographs of cross-sections of sintered Mg<sub>2</sub>Si samples with and without  $\beta$ -FeSi<sub>2</sub> films after heat treatment in air at 600 °C for 1–3 h: (a) without  $\beta$ -FeSi<sub>2</sub> films for 1 h; (b) without  $\beta$ -FeSi<sub>2</sub> films for 3 h; (c) with  $\beta$ -FeSi<sub>2</sub> films for 1 h; and (d) with  $\beta$ -FeSi<sub>2</sub> films for 3 h.

of oxygen at 600  $^\circ\text{C}\textsc{,}$  and it improved the oxidation-resistance of  $Mg_2Si.$ 

4. Conclusions

Above 450 °C, Mg<sub>2</sub>Si reacts with O<sub>2</sub> in air to yield MgO and Si. The Avrami exponent (*n*) is equal to ~0.5, and it depends on the reaction temperature and time; this indicates that the oxidation is controlled by the diffusion-controlled reaction. In order to improve the oxidation-resistance of Mg<sub>2</sub>Si,  $\beta$ -FeSi<sub>2</sub> films were fabricated on sintered Mg<sub>2</sub>Si samples by RF magnetron-sputtering deposition at RT followed by post-annealing at 600 °C in vacuum. An oxide layer having a thickness of 8 ± 3 µm was observed on the uncoated Mg<sub>2</sub>Si samples after heat treatment in air at 600 °C for 3 h. However, no oxide layer was formed on Mg<sub>2</sub>Si samples coated with 0.7-µm thick  $\beta$ -FeSi<sub>2</sub> films. The  $\beta$ -FeSi<sub>2</sub> layer effectively prevented the diffusion of oxygen at 600 °C and improved the oxidation-resistance of Mg<sub>2</sub>Si.

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